

Hjälpmödel: Ett A4-ark med godtyckligt innehåll (handskriven, datorutskrift, diagram, m.m.).

Kontrollskrivningen har 2 tal, med totalt 10 poäng. Den omfattar del B i kursen, 'Transient', och motsvarar del B i tentamen. Betyget på tentan kommer att inkludera del B genom att ta det högsta av betygen från KS2 (den här) och från tentans del B. Del B är godkänt vid $\geq 40\%$, men glöm inte att tentan kräver 50% räknat över alla delarna.

Var tydlig med diagram och definitioner. Lösningar ska uttryckas i kända kvantiteter, och förenklas. Kontrollera svarens rimlighet genom t.ex. dimensionskoll eller alternativ lösningsmetod.

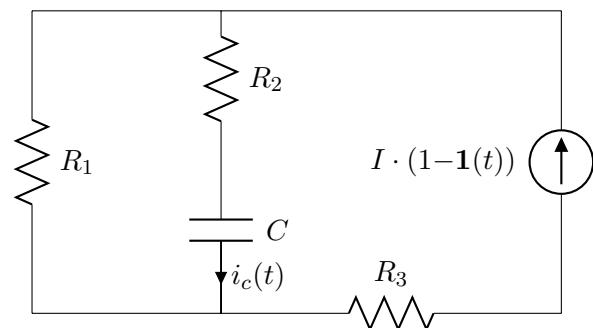
Använd återstående tid för att kontrollera svaren!

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1) [5p]

Bestäm strömmen $i_c(t)$ i kondensatorn som tidsfunktion för perioden $t > 0$.

Kretsen kan antas vara i jämviktsläge innan tiden $t = 0$. Observera att enhetsstegfunktionen är skriven här som $\mathbf{1}(t)$. Alla markerade komponentvärdet är kända.



2) [5p]

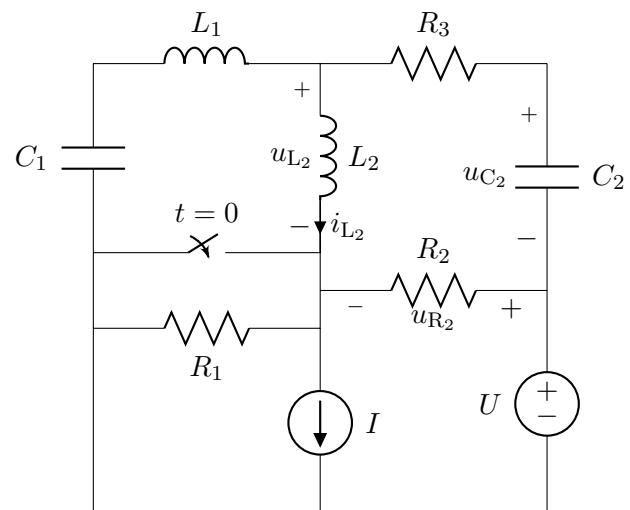
Alla markerade komponentvärdet är kända, t.ex. L_1 , U . Alla markerade spänningar och strömmar är okända, t.ex. u_{R_2} . Brytaren stänger vid tid $t = 0$.

a) [3p] Betrakta jämviktsläget innan brytaren stänger, d.v.s. $t = 0^-$.

Bestäm i_{L_2} , u_{R_2} och u_{C_2} .

b) [2p] Betrakta tiden direkt efter att brytaren stänger, $t = 0^+$.

Bestäm u_{L_2} och u_{R_2} .



Tänk på att rita om kretsen med rätt information för fallet som du analyserar. Dubbelkolla omritningen. Var systematisk. Var tydlig med var slutsvaren är!

Solutions, KS2

1)

The current source is $I \cdot (1 - \mathbf{1}(t))$, which means it is I for $t < 0$ and 0 for $t > 0$.

In the equilibrium, the state (continuous variable) of the capacitor is $u_c(0^-)$. The value can be found by setting the capacitor to be an open circuit: then all current I passes through R_1 , and no current passes through R_2 , so the voltage across the open-circuited capacitor is IR_1 .

At $t > 0$ the “zero current source” can be seen as an open circuit, so the branch on the right side can be ignored. The capacitor voltage is initially $u_c(0^+) = u_c(0^-) = IR_1$. The final value of capacitor voltage will be zero, as the capacitor is connected in a loop with R_1 and R_2 . You could reason about why this means it will discharge, or you could just see the two as a Thevenin source with zero voltage, and consider that the equilibrium voltage of a capacitor connected to a Thevenin source is the open-circuit voltage of the source.

We can find the equation for capacitor voltage by the equivalent-circuit method or by writing the equation. It will be

$$u_c(t) = IR_1 e^{-\frac{t}{C(R_1+R_2)}}$$

But the *current* is requested; it has been defined with passive convention relative to the voltage, so we have $i_c(t) = C \frac{du_c(t)}{dt}$. Therefore,

$$i_c(t) = -\frac{CIR_1}{C(R_1 + R_2)} e^{-\frac{t}{C(R_1+R_2)}} = -\frac{IR_1}{R_1 + R_2} e^{-\frac{t}{C(R_1+R_2)}}.$$

This tells us that the current comes out of the top of the capacitor, first quickly (at $t \simeq 0$, when the capacitor has a voltage $\simeq IR_1$), then slower and slower as the capacitor discharges.

The result could instead have been found by considering initial and final values of the current, or by finding and solving a differential equation for the current.

2)

Quick answers, for anyone who wants to check. Please think about any differences, and try to understand why they exist ... one or both of us is presumably wrong....

a) Equilibrium, before the switch closes: $t = 0^-$.

$$* i_{L_2} = 0$$

This is because all paths through L_2 are blocked by a series capacitor (open circuit in equilibrium).

$$* u_{R_2} = U - \frac{(U - IR_2)R_1}{R_1 + R_2} = \frac{U(R_1 + R_2) - (U - IR_2)R_1}{R_1 + R_2} = \frac{(U + IR_1)R_2}{R_1 + R_2}$$

This is from nodal analysis (or other method) on the lower part of the circuit, after identifying that the capacitors block all current in the upper part.

$$* u_{C_2} = -u_{R_2} = \frac{(-U - IR_1)R_2}{R_1 + R_2}$$

This is seen from the fact that C_2 causes R_3 to have no current, and therefore no voltage, and L_2 is treated as a short-circuit. There is therefore the same voltage across C_2 and R_2 , but the definitions are in opposite directions.

b) Continuity, immediately after the switch closes: $t = 0^+$.

$$* u_{L_2} = U + u_{C_2}(0^+) = U + u_{C_2}(0^-) = U - \frac{(U + IR_1)R_2}{R_1 + R_2} = \frac{(U - IR_2)R_1}{R_1 + R_2}$$

There is still no current in R_3 , as the only path through it passes through inductors (L_1 in one way, L_2 in the other) which still have zero current at $t = 0^+$. Taking KVL around the loop of the switch, U , C_2 , R_3 and L_2 , we find that $u_{L_2} = U + u_{C_2}$, leading to the above.

$$* u_{R_2} = U$$

Notice that R_2 is now in parallel with the voltage source.